

DYNAMIC ANALYSIS OF HIGH RISE NORMAL AND UNSYMMETRICAL STEEL BUILDING WITH ECCENTRIC BRACING SYSTEM

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Abstract: To solve practical problems and to comprehend real characteristics of soils and construction having BRB also without BRB designs, 12 models were developed utilizing different forms of bracing and soil types. It includes X bracing, V bracing, Y bracing, and bracing without BRB, as well as three types of soil: sand, silt, and clay, each of which will produce four models, for a total of 12 models. Buildings with a height of 21 meters and seismic zone 4 have been considered. The earthquake load combination will be based on multi-story steel frames with and without BRBs. It is studied using ETABS17 and linear dynamic analysis. The results show how various characteristics of the structure, such as story displacement, story drift, story stiffness, and story shear, change in response to seismic excitation and seismic forces. According to the findings, story displacement, story drift, and story stiffness all vary dramatically when the soil type varies, and different forms of BRB help significantly to withstand distortion. As a result, soil structure interaction in combination with X BRB must be favored over seismic excitation.

I INTRODUCTION

1.1 General

The SSI refers to the practice wherein the soil's reaction affects the structure's motion and the structure's motion effects the soil's response. Neither the structural nor the variables are expected to change are autonomous of one other in this instance. Steel multi-story frames are a common construction structure. Installing buckling-restrained bracing (BRBs), which are renowned for their high energy dissipation capacity, may help individuals who have inadequate seismic protection. BRBFs, on the other hand, are often chastised for having significant leftover abnormalities after tremors, which obstruct post-event repair work and rapid occupancy. These, which were developed with the specific goal of reducing residual deformation for protected buildings, have advanced rapidly in recent years. As a result, the goal is to create a BRB by combining these two distinct braces. To find the best option, three Shapes BRBs are suggested. Through linear dynamic calculations, the micro steel frames fitted with BRB are method of data analysis. Inter storey drift proportions, inter storey movement, and shear forces are the seismic response characteristics of interest.

The term "soil-structure interaction" may be described as "the effect of the behavior of the soil immediately under and surrounding the foundation on the reaction of the soil-structure when exposed to static or dynamic stresses."

Soil-structure interaction, or SSI, may have a significant influence in the dynamic features of structural reactions, particularly for large buildings built on relatively soft soil. Soil-structure interaction is ignored in traditional structural analysis,

and structural reactions are only taken into consideration. Despite the fact that the impacts of soil flexibility on vibrating systems such as machine foundations have previously piqued the interest of a number of academics, the history of SSI research dates back to the late 1970s. Nuclear power plants, as investigated by Idriss et al. (1979) and Johnson, were the first places where SSI seemed to have a significant impact on structural response (1981). Extensive study has been done in recent decades on the impact of shallow root (SSI) on the structural response of constructions. It was discovered that when soil and structure interact, the primary frequencies of the response decreases and the energy dissipation changes, which is related to radiated and substance damping in the soil. Johnston is a town in the state of New (2003). Despite recent research on BRB crossings and structure demonstrating the efficacy of SSI on structural response of the systems, the typical practice generally overlooks the impacts of SSI on earthquake loading of BRB structures, relying on the elasticity of BRB buildings. As a result, SSI may be required to be addressed in the designing of a platform structure, not just for seismic reasons but also for economic reasons. In recent years, a number of academics have been interested in the combined impact of SSI and the BRB on buildings. The interaction of soil and structure has mostly been studied for base-isolated bridges, liquid storage tanks, and multistory structures.

A foundations is a structure that connects the superstructure to the surrounding soil or rock. Only the vertical loads of the structure must be transferred to the supporting rock under static circumstances. In a seismic environment, the stresses placed on a foundation by a structure during seismic excitation may much

beyond the static vertical loads, causing uplift; there will also be horizontally forces and potentially displacement at foundation level. The soil and rock at the location have unique properties that may greatly magnify the incoming earthquake movements from the earthquake source.

The behavior of both the structure and the soil, as well as their interaction, must be addressed by the foundation designer. The interface problem is crucial in many civil engineering settings, because it encompasses a broad range of issues. These studies cover shallow and deep foundations, floating structures, retaining wall-soil systems, tunnel linings, and earth structures, among others.

The goal of this study is to examine the tectonic activities of various “ systems in steel structures. The analysis of a multi-story building with soil structural interaction will be presented in this study. With the assistance of software, a three-dimensional modeling and study of the structure will be carried out. All constructions will be subjected to equivalent static assessments. The shaking table test will be used to compare this analysis to a realistic model of a multi-story structure. The BRB damping system is considered in this study, and it is compared to a basic model.

1.2 Buckling restrained braces (BRB)

In the area of lateral force resisting constructions, Buckling-Restrained Brackets (BRBs) are a modern invention. A basic tasks is a kind of structural system that is frequently employed in constructions that are subjected to lateral loads like wind or earthquake pressure. A braced frame's members are usually constructed of stainless components, which can operate in both tension and compression.

Vertical loads are carried by the frame's beams and columns, while lateral loads are carried by the bracing system. Brace placement, on the other hand, may be troublesome since it can compromise with façade's design and the placement of openings. Bracing has been expressed as an interior or exterior design element in buildings with high-tech or post-modernist designs.

1.2.1 Types of Bracing

The most frequently utilized bracings are examined and categorized based on their form.

1 Single Diagonal Bracing

Only one leg is used in this kind of bracing to withstand the lateral displacement caused by major earthquake. It is very effective at resisting unidirectional forces.

2. Cross-Bracing or X-Bracing

Two diagonal elements cross one other in cross-bracing (or X-bracing). These simply need to be tension-resistant, with one brace resisting sideways pressures at a time, depending on the loading direction.

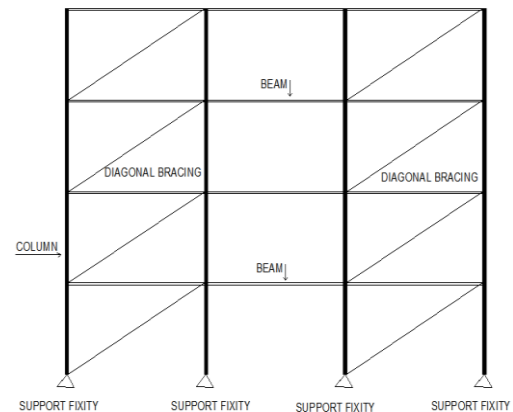


Figure 1.1: Diagonal Bracing

3. V-Bracing

Two diagonal members, in the form of a V, stretch first from two leading corner of a frame structure and intersect at a Center point at the bottom horizontal member. The compression brace's buckling capacity is likely to be considerably lower than the tension brace's tension yield capacity.

4. Inverted V-Bracing

The two elements of inverted V-bracing (also called as chevron brace) meet at a center point on the top horizontal member. The procedure is similar to V bracing.

Aim and Objective of the Study

The goal of this study is to examine the functional performance of a steel frame utilizing different forms of BRB systems while considering the interaction of soil and structure during seismic excitation, with the following goals in mind.

- 1) ETABS17 was used to calculate the seismic behavior of a multi - story steel structure with BRB Damping system.
- 2) To research various kinds of braces and determine the most effective bracing method for improving steel frame construction characteristics.
- 3) Factors that may contribute to G+6 story buildings using X brace, V bracing, and Y bracing modeling in various soil conditions such as clay, silt, and sandy to determine precise variations by considering natural soil interactions into account.
- 4) To compare parameters obtained from steel frame seismic analysis with values obtained from displacement, story drift, and base shear.
- 5) To determine the efficacy of a damping system in

improving the structural integrity of an earthquake-resistant construction.

- 6) Make recommendations on how to enhance the structural stability in the event of a seismic event.

System development

Many studies on earthquake loading including assessment of BRB have been conducted utilizing various theories, techniques, and tests. The research, as shown in the literature, develops various new methods, but there is still room for various parameters to be taken into account, such as structural behavior, ground isolation, elastic bearing, and many others, so the effect of the BRB system is taken into consideration in this study. The performance of a steel frame with BRB under earthquake excitations may be susceptible if soil structure interaction is not taken into account. We may get accuracy for seismic results by selecting the appropriate variable as well as modeling for fulfilling the safe design.

II PROBLEM STATEMENT AND

METHODOLOGY

2.1 Introduction

The primary goal of this research is to look at the behavior of a steel frame building's bracing system. Linear dynamic analysis is used to examine twelve different situations. The assessment is conducted with the aid of the ETABS17 program.

2.2 Problem Statement

To solve the practical issues and to comprehend the real characteristics of soils as well as construction utilizing BRB or without BRB models, 12 models will be built utilizing different brace forms and soil types. It will include X bracing, V bracing, Y bracing, and bracing without BRB, as well as three types of soil (sand, silt, and clay), each of which will provide four models, for a total of 12 models to be performed. Earthquake zone 4 will be considered for the building, which is a G+6 storey with a height of 21 meters. The effects of earthquake load combinations on micro trusses with and without BRBs are studied using ETABS17 linear dynamic calculations. The results show how various characteristics of the structure, such as story displacement, story drift, story stiffness, and story shear, change in response to seismic excitation and seismic forces.

2.3 Design data

Model 1- levels are built according to the concept of state design. Since IS 456:2000 also uses limit state techniques, whenever it applies, it has been followed. The design should provide a sufficient level of security and structural serviceability. Therefore, the structure for eventual as well as maintainability limits should be inspected.

2.4 Software Development ETABS 2017

Computers systems Structural, Corporation (CSI), an Architectural and Seismic Engineering Company, has created a program for structural design in ETABS. ETABS 2017 is a final element software for a broad purpose which carries out the structural systems static or dynamic analysis, whether linear or nonlinear. It is also a strong tool for designing AASHTO, ACI and AISC planning laws buildings. ETABS 2017 is a comprehensive software for the simplest issues or for the most difficult projects. It has an unrivaled powerful, easy-to-use and productive graphical user interface.

2.5 Soil Structure Interaction

Soil structure Soil In the conduct of foundations, interaction plays an essential role. It is extremely necessary to examine the deformed properties of soil and the flexural properties of the foundation for constructions such as beams, piles, mat foundations and box cells. It can be observed that the actual design values come in very different from those developed without regard to interaction when interaction is being taken into consideration. In most cases, contact generally results in a decrease of critical shear design values and moments etc. There may nevertheless be a number of places in which the levels are increasing. Due to these opportunities, the economy and structural security play their own part

Various investigations showed that contact with superstructure may significantly influence the max deflections of a substructure raft or beam. In certain instances, the reduction is as great as 80%. The stiffness of the raft relation to soil is very high in relatively stiff rafting compared to flexible rafts for bending moments. The same tendency is also evident from an elastic plastic analysis even though to a considerably lower extent. The most serious cause of cracking and possibly superstructure collapse is an equal settling. The stiffness of the superstructure contributes to the reduction of differential settlements. Naturally, only interactive analysis must be conducted to achieve this.

2.6 Soiltest:

for low-level sub-structures, borehole depth may very well be specified to about 6 m just below expected simple level, with at most one borehole continuous deeper to less than 30 m, lower subterranean or rejected size. For subterranean buildings, at minimum one soil boore should be indicated for per 230 square metres. Over twelve metres, or over three storeys. Borsings should bepacedatlesstan15m intervals for big subterranean structuresfoundedonpoorsoils. It is suggested that at least five borings be placed, one in the middle and the others at subterranean corners.

2.7 Concept ofBRB

Buckling Constrained Reinforced concrete Framework is a technologically sophisticated form of CBF that includes the effects of lateral stresses under the structure. Buckling is the most advanced type of CBF The BRBF represents the state-of-

the-art in braced frame design as a technology released at the end of 1990. The most important components of the hinged retained strap are steel core, layer and housing avoiding binding as illustrated in Figure

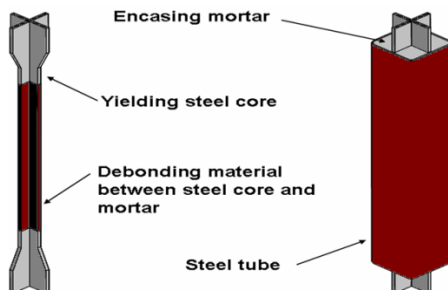


Figure 1. Steel core, bond preventing layer and casing

The necessary strength of the framing components also makes the system comparable to the weak connection: beams and columns must be sized to withstand strengths which match the anticipated strength of the braces incorporating stress hardening variables and other excess strength sources. Careful designers should also include bracing over the building height to limit the drift levels by carrying out dynamic analyzes and using a tiny fraction of the necessary strength to size braces.

The inclusion of BRBF in the designer summary of the key technologies is increasingly important when design and performance problems with traditional braced frames are addressed (CBF). Re focuses on the appropriate design and details of strap structures to overcome possible limits on their ductility. Review of current testing and review of previous testing led to renewed emphasis. The core of steel is built to withstand the axial forces of the bracing. Bond prevention disconnects the core and the cabinet. This enables the steel core, which grow in bracing, to withstand complete axial forces. Case offers side support against theoretic bending.

2.8 Method of Seismic Analysis

A. Static Equivalent Method: The lateral design force is computed after an earthquake

1. Sismic coefficient horizontal design:

For a construction the horizontal seismic design coefficient A_h should be as follows:-

$$x (I/R) \times (S_a/g) [Z/2/10]$$

Provided A_h 's value is not smaller than $Z/2$ for any t-structure than 0.1s regardless of I/value. R's

Where,

Z = Factor of zone.

I = factor of importance, based on the structure's functionality.

R = Factor to reduce response based on earthquake damage perceived Structural performance.

Its $/g$ = Coefficient of average reaction.

2. Seismic Shear design:

The overall lateral strength or seismic base shear (V_b) of the design along every major direction is as follows:

$$A_h.W = A_h.$$

Where, W is the building's seismic weight.

3. Design force distribution:

The calculated design base shear (V_b) is distributed at the building height as follows:

$$Q_i = V_b(w_i h_i^2 / \text{total}) \quad Q_i = V_b$$

Where,

Q_i = Lateral strength design at each floor level I

W_i = floor sismic mass i .

H_i = floor height from the base I measured.

2.9 Response Spectrum Method

This technique is often referred to as a modal or modal way of overlaying. The technique applies to those structures in which non-basic modes substantially influence the structure's response. The study of stresses including deflections in multi-story structures due to medium-intensity ground shaking is particularly useful, which results in a fairly significant but basically linear reaction in the structure. Calculative benefits exist for predictions of deformations and members' forces that use the frequency response technique of seismic analysis in structural systems. The technique includes calculating just the average of many seismic movements with the maximum displacement values and the force of the member in every mode using the smooth spectrum.

Just one type of vibrations has been addressed in the seismic coefficient technique (one mode method). The timeframe for this pattern was extremely simple without the unrestricted study of vibrations. The natural phases and modes acquired with free vibrational analysis are utilized in response spectrum methods to achieve seismic strength. The maximum reaction of the hypothetical single-degree free system during seismic movements, with a given period and damping. The maximum response is determined in terms of peak 's lead, maximum operating velocity or highest mean shift and for different damping levels.

Sufficient mode counts are to be utilized so as to make upwards of 90% of the overall object 's mass of the modal mass of the modes examined. The seismic shaking impact may therefore be measured at each node of the discrete structural model as concentrating earthquake pressure gradient and time corresponding to their translational and rotational levels of

NO	SOIL CONDITIO N	BRACING
1	CLAY	Without Bracing
2		X bracing
3		V Bracing
4		Y Bracing
5	SAND	Without Bracing
6		X bracing
7		V Bracing
8		Y Bracing
9	SILTY	Without Bracing
10		X bracing
11		V Bracing
12		Y Bracing

freedom. These seismic forces and moments are supported by every mode of Vibration.

1. Each level in each mode model is designed forces:

Q_{ik} = Kingdom of God. W_i Where, A_k = Horizontal design of spectrum acceleration value

$\sum F_i$ = fashion form of floor I in fashion k

W_i = floor sismic mass i.

P_k = Factor modal involvement.

2. Shear story strength in every mode:

Acting in history I is presented in mode k

$$V_{ik} = \sum_{j=1}^n Q_{ikn} j = i+1$$

Shear force because of all examined modalities. The peak story shearing force (V_i) in history I is produced by combining them by different techniques, including SRSS, CQC or relative sum approaches, etc., owing to the distinct modes.

III SOFTWARE ANALYSIS

For the smallest issues or the most complicated undertakings, ETABS17 refers for Expanded Three-dimensional Building System Analysis.

3.1 Modeling in ETABS17

Because of its flexibility in the consideration of forbidden geometry, loading, water stress and change in material characteristics, ETABS17 is ideal for the study of building construction structures such as high-speed buildings, tower buildings, multi story buildings, circular tanks, etc. A variety of

models and analyzes have been created which are successful and economically computational in various circumstances in practice.

IV RESULTS

The real behavior of the soils and structures must be considered with BRB and without a BRB model to solve the practical problems. The research is focused on the reaction of the steel frame model to lateral excitation so that 12 models are produced using different forms of bracing as well as soil type. It has X bracelet model, V bracelet, Y bracelet model and sans BRB with 3 soil type, sand clay minerals every makes up 4 models, with a total of 12 models to execute. It is believed that the building consists of G+ 6 storeys, 21 m tall and seismic area 4. On multi-story structural members with BRBs and without linear and dynamic analysis using ETABS17, earthquake load combinations will be taken into consideration. Tale displacement, story shaving, story twisting and story rigidity is the parameter to be examined.

4.1 Results for clay soil

Various forms of the seismic reaction of the BRB System with clay floor in terms of history displacement, historical drift, narrative shear and history rigidity are shown.

Move Story Story Clay Soil

The lateral displacement of a storey changing in the EQ-x and EQ-Y direction from Table 5.1 to Table 5.2. V bracing, Y bracing without clay soil bracing.

Move Story Story Clay Soil

The narrative laterally differentiated from X bracing, V bracing, Y stracing and no bracing for clay are shown in EQ-X and EQ-Y directions from Table 5.1 to Table 5.2.

Story DisplacementEQ-X

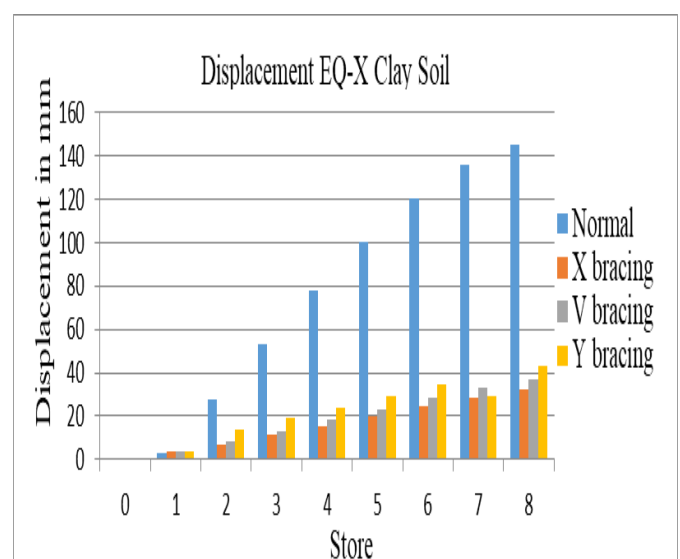


Figure 1: Story Displacement EQ-X Clay Soil

Table .1: Story Displacement EQ-X Clay Soil in mm

Table 5.1: Story Displacement EQ-X Clay Soil in mm

Story	NORMAL	X BRACING	V BRACING	Y BRACING
8	144.8	32.5	37	43
7	135.8	28.75	32.95	28.95
6	120.5	24.57	28.29	34.29
5	100.64	20.144	23.26	29.26
4	77.76	15.627	18.06	24.06
3	53	11.21	12.9	18.9
2	27.61	7.08	7.97	13.973
1	3.03	3.48	3.573	4
0	0	0	0	0

Table 2: Story Displacement EQ-Y Clay Soil in mm

Table 5.2: Story Displacement EQ-Y Clay Soil in mm

Story	NORMAL	X BRACING	V BRACING	Y BRACING
8	68.20	29.00	31.58	37.5
7	62.89	25.91	28.2	34.4
6	55.29	22.15	24.18	30.16
5	45.67	18.03	19.75	25.75
4	34.65	13.76	15.10	21.10
3	22.93	9.50	10.43	16.45
2	11.5	5.38	5.87	8
1	2.22	1.96	2.1	2.5
0	0	0	0	0

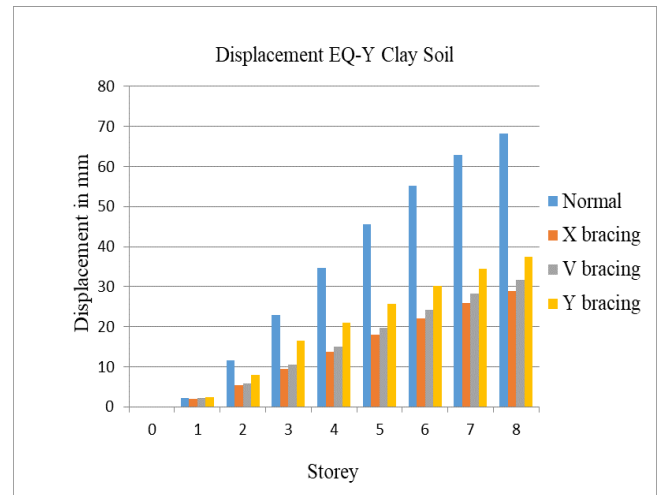


Figure .3: Story Displacement EQ-Y Clay Soil

• **Story Drift ClaySoil**

In the EQ-X and EQ-Y direction, a side deformation of the soil between the stories varies with X brace, V brace, Y brace and no clay bracing is illustrated.

Story DriftEQ-X

Table3 : Story Drift EQ-X Clay Soil in mm

Story	NORMAL	X BRACING	V BRACING	Y BRACING
8	8.97	3.75	4.068	4.05
7	15.3	4.176	4.656	4.66
6	19.86	4.43	5.03	5.034
5	22.881	4.518	5.2	5.21
4	24.663	4.416	5.16	5.17
3	25.488	4.130	4.926	4.928
2	24.651	6.27	7.06	9.9
1	2.89	3.18	3.15	4
0	0	0	0	0

Table5.4: Story Drifts EQ-Y Clay Soil in mm

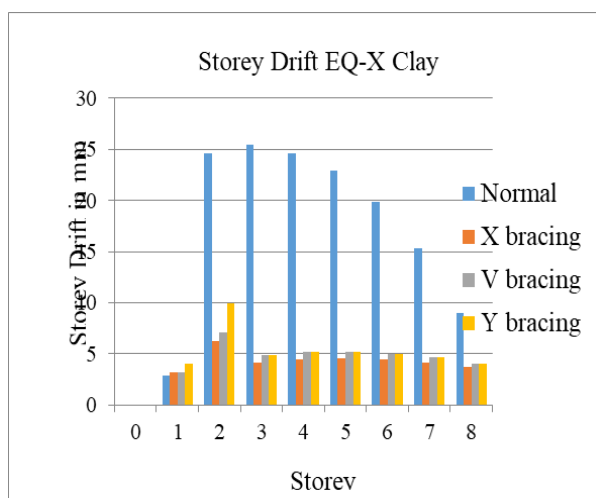


fig2. Story Displacement EQ-Y

Story	NORMAL	X BRACING	V BRACING	Y BRACING
8	5.3	3.189	3.369	3.38
7	7.6	3.759	4.02	4.03
6	9.6	4.113	4.437	4.4
5	11.02	4.278	4.65	4.7
4	11.71	4.3	4.67	4.8
3	11.43	4.11	4.56	8.43
2	9.315	4.26	4.65	5.5
1	2.03	1.59	1.62	2.5
0	0	0	0	0

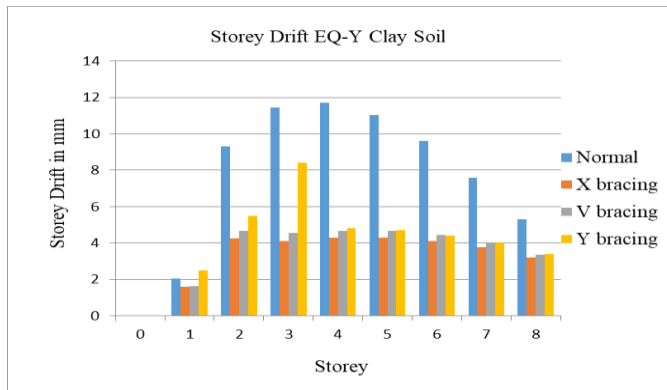


Figure .4: Storey Drift EQ-Y Clay Soil

• **Story Shear for Clay Soil**

In EQ-X and EQ-Y direction, lateral storey shear floor pattern with X brace, V braced, Y braced and no clay braced are illustrated.

Story shear EQ-X

Table.5: Story Shear EQ-X in kn

Story	NORMAL	X-BRACING	V-BRACING	Y-BRACING
8	356.5	527.59	492.27	462.27
7	625.00	798	762	732
6	817	990	954	924.5
5	944	1138	1082	1051
4	1020	1194	1158	1128
3	1058	1232	1196	1166
2	1070	1285	1249	1219
1	1071	1325	1289	1259
0	0	0	0	0

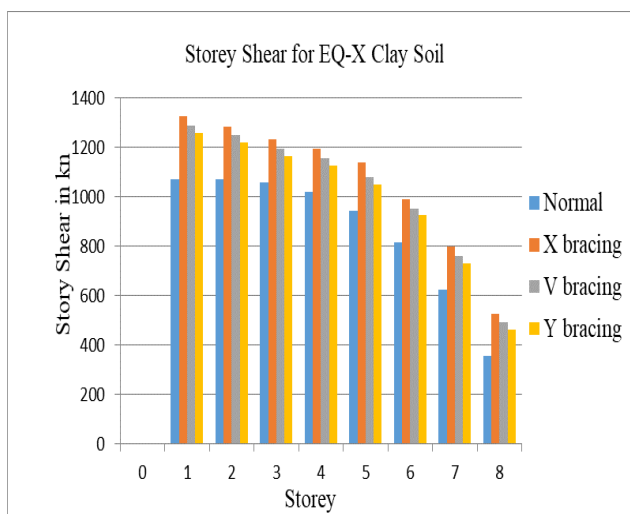


Figure 5.: Story shear for EQ-X Clay Soil

Table6: Story Shear EQ-Y in kn

Story	NORMAL	X-BRACING	V-BRACING	Y-BRACING
8	243.5	365.5	335.2	315.27
7	515	636	605	585.3
6	704	828	797.5	777.6
5	831	976.3	925.1	905
4	907	1032	1001	981
3	945	1070	1039	1019
2	957	1108	1077	1047
1	958	1144	1113	1078
0	0	0	0	0

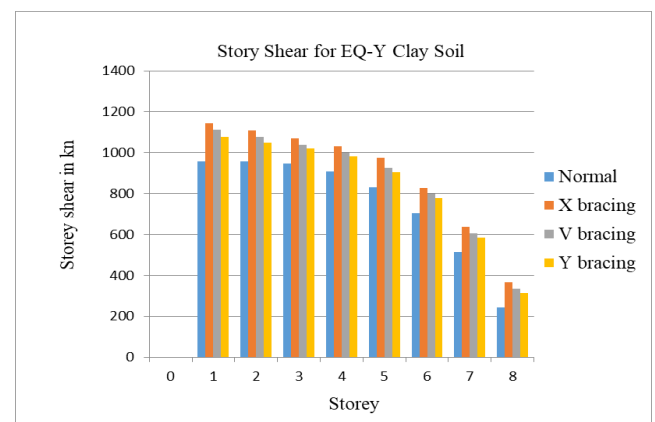


Figure 6: Story Shear for EQ-Y Clay Soil

• **Story Shear for EQ-Y**

• **Story Stiffness for Clay Soil**

Lateral stiffness with X braces, V braces, Y braces and no bracing are demonstrated for clay flooring

Story Stiffness for EQ-X

Table 7: Story Stiffness EQ-X in kn/m

Story	NORMAL	X-BRACING	V-BRACING	Y-BRACING
8	39626	95253	87852	80451
7	40889	150425	134750	119075
6	41141	185117	162835	140553
5	41270	209992	182098	154204
4	41367	232129	198331	164533
3	41511	257275	215398	173521
2	43511	218088	187399	156710
1	380955	547382	540686	533990
0	0	0	0	0

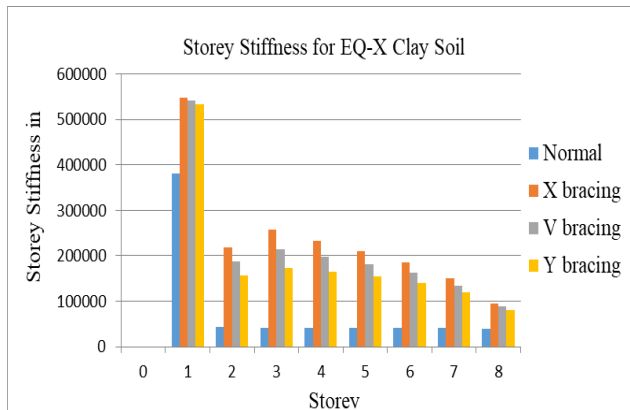


Figure 7: Storey Stiffness for EQ-X Clay Soil

Table.8: Storey Stiffness EQ-Y in kn/m

Story	NORMAL	X-BRACING	V-BRACING	Y-BRACING
8	67213	112149	106074	100000
7	82665	167079	156050	145022
6	84922	199505	184650	169795
5	85631	221743	203759	185776
4	87107	240695	219404	198113
3	92530	258029	232692	207355
2	115260	279897	255765	231633
1	534995	829975	793853	757730
0	0	0	0	0

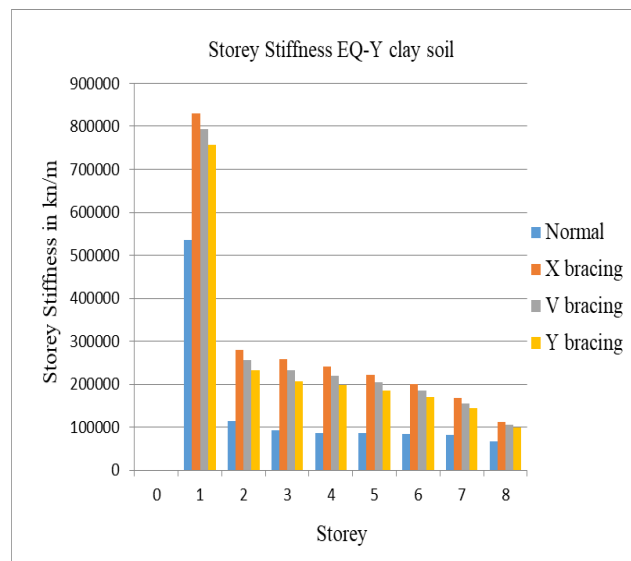


Figure 8: Storey Stiffness EQ-Y clay soil

As for clay soil we get results. The same method applies to get silty soil as well as sandy soil results.

V COMPARATIVE RESULTS:

Overall comparison findings are presented in terms of story, story drift, base shear, and story stiffness in all three kinds of soil with various forms of seismic BRB system reaction.

Maximum Story Displacement

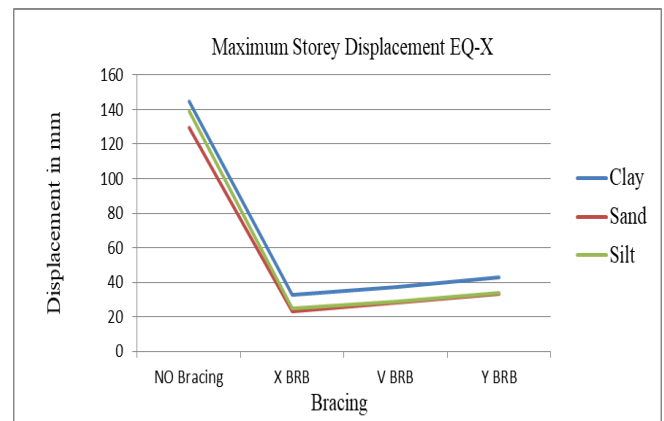


Fig 9. Maximum Story Displacement EQ-X

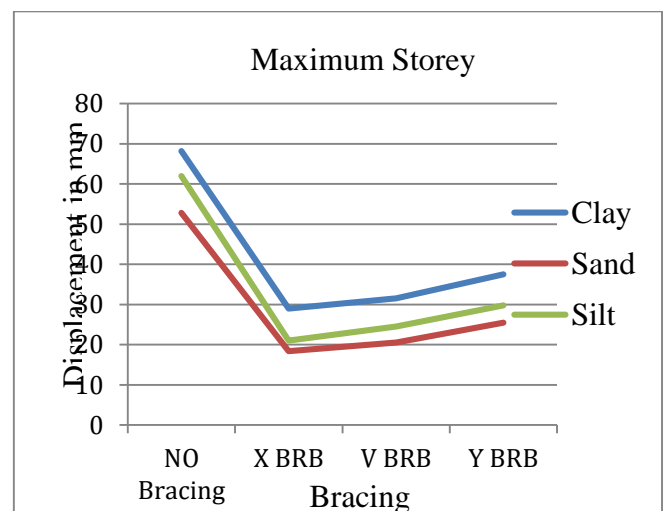


Fig10. Maximum Story Displacement EQ-Y

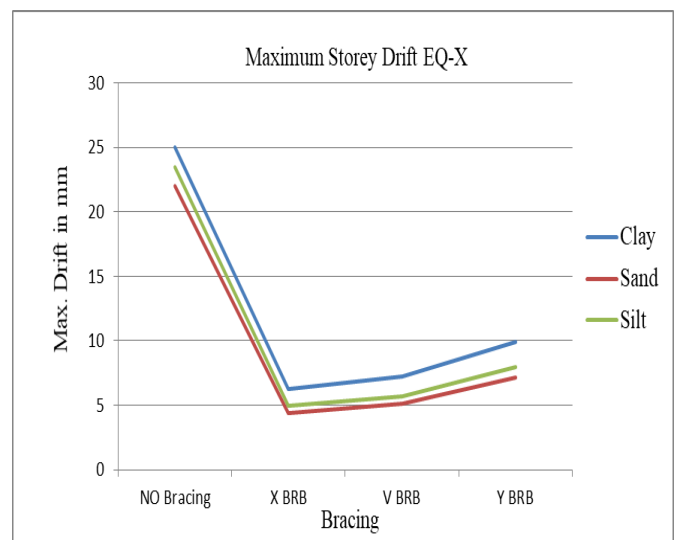


Fig11 . Maximum Story Drift EQ-X

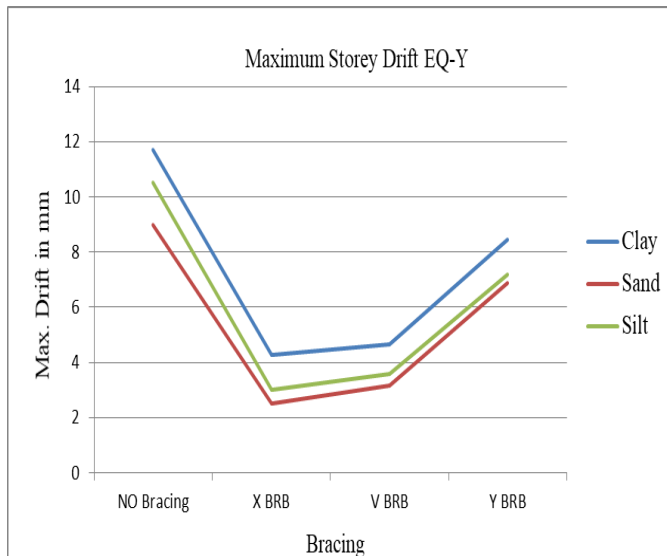


Fig.12 Maximum Story Drift EQ-Y

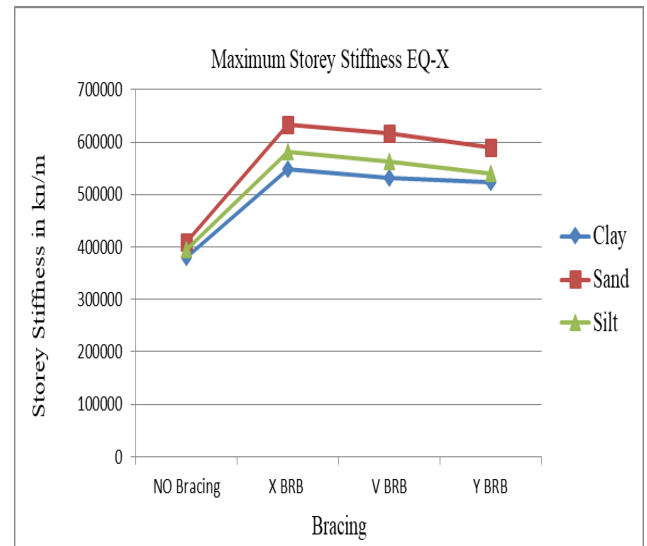


Fig. 15 Maximum Story Stiffness EQ-X

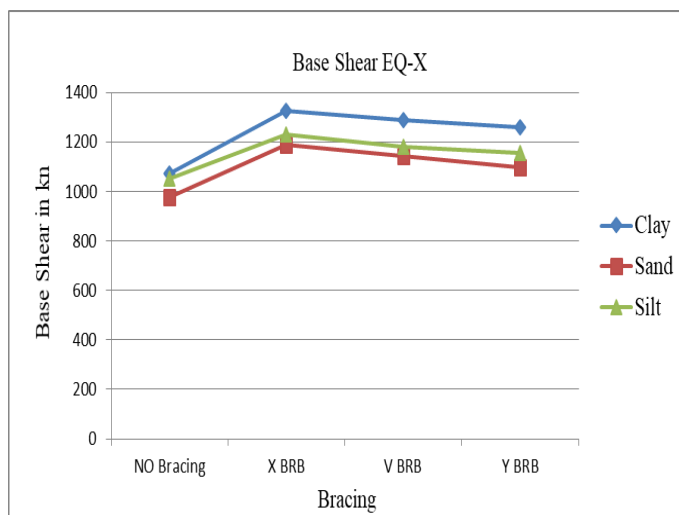


Figure13: Base Shear EQ-X

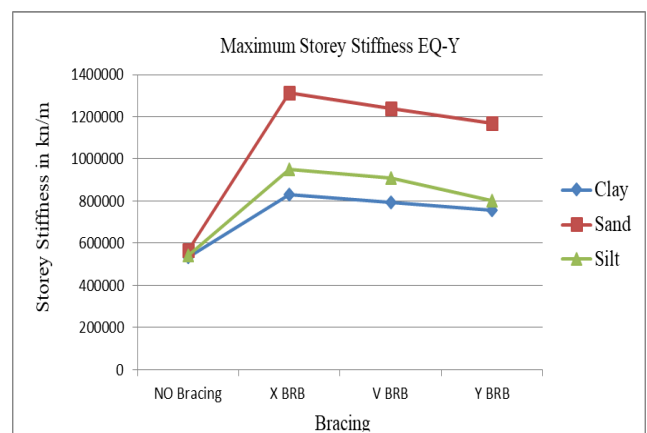


Fig16. Maximum Story Stiffness EQ-Y

VI CONCLUSION

6.1. Introduction

Different forms of the BRB system have been used to structure the structural performance of the steel framework building in seismic arousal. For findings and computations, software analyzes utilizing ETABS17 are produced. The seismic load is accomplished using response spectrum technique in line with IS 1893(2016). Different conclusions are drawn in the next part in line with the preceding findings and discussion chapter. The building is investigated in the research and drawn from the aforesaid study with different combinations of BRB in consideration of SSI.

6.2. Conclusions

1. In the X structural members in clay and in the sandy soil story displacement reduction by 30% and the Y bracing decreased by 16% and the V decrease by only 11% compared with the standard frame.
2. Base shear following comparison with the interaction

between soil structure X and Y direction, it has been shown that the next X brace clay soil varies between 15 percent -20 percent for various soil and base shear.

3. After comparing the interaction of the narrative drift either with or without healthy soil in X and Y, it was found that story drift varies from 15% to 40% in various stories. Story drift Therefore it may be inferred that for higher areas, multi-story buildings and poor soils, SSI should be considered.
4. The finest performed X bracing may be to limit released in any soil.
5. The self-weight deformity of soil structure interactions is found 16% greater.
6. Operation of the whole X brackets is good than V and Y BRB and the interaction between the soil structure lets us track the real comportement of the frame system.

Future scope

The same job may be done by maintaining the impact of changes in the slope for rear structures using bracing system. Studies to determine the appropriate location of bracings for various configurations may be pursued further. The same process may be done with the isolation system and various damper.

7. References

[1] Hector Guerrero, Experimental damping on frame structures equipped with buckling restrained braces (BRBs) working within their linear-elastic response, *Soil Dynamics and Earthquake Engineering*, 20 December 2017, pp 196 to 203.

[2] F. Barbagallo, Seismic design and performance of dual structures with BRBs and semi-rigid connections, *Journal of Constructional Steel Research*, 31 March 2019, pp 306 to 316.

[3] M. Bosco, M. Marino, Design of steel frames equipped with BRBs in the framework of Eurocode, *Journal of Constructional Steel Research*, 7 May 2015, pp 43 to 57.

[4] S.A. Seyed Razzaghi, Evaluating the Performance of the Buckling Restrained Braces in Tall Buildings with peripherally Braced Frames, *Journal of Rehabilitation in Civil Engineering*, 5 February 2018, pp 21 to 39.

[5] Antonios Flogeras, The seismic response of steel buckling-restrained braced structures including soil-structure interaction, *Earthquake and Structures*, March 2017, pp 45 to 63.

[6] Songye Zhu, Seismic Analysis of Steel Framed Buildings with Self-Centering Friction Damping Braces, 4th International Conference on Earthquake Engineering 2006, Vol. 14, pp 12-17.

[7] Rodolfo Antonucci, Shaking Table Testing of an RC Frame with Dissipative Bracings, 13th World Conference on Earthquake Engineering Vancouver, Vol. 13, March 2017

[8] Chien-Liang. Lee, An Experimental Verification of Seismic Structural Control Using in-Plane Metallic Dampers, *International Journal of Structural and Civil Engineering Research*, August 2018, pp 3 to 11.

[9] Marco Baiguera, Dual seismic-resistant steel frame with high post-yield stiffness energy-dissipative braces for residual drift reduction, *Journal of Constructional Steel Research*, May 2015, pp 198 to 212.

[10] Nefize Shaban, Shake table tests of different seismic isolation systems on a large scale structure subjected to low to moderate earthquakes, *Journal of Traffic and Transportation Engineering*, 7 October 2018, pp 480 to 490.

[11] G. Palazzo, Damping Coefficient Of A Building With BRB Subject To Three Types Of Earthquake Ground Motions, 16th World Conference on Earthquake Engineering, 16 January 2017.

[12] Agarwal P. and Shrikhande M. (2006) "Earthquake resistant design of structures", Prentice- Hall of India Private Limited, New Delhi, India.

[13] Gustavo L. Palazzo, A Steel Moment-Resisting Frame Retrofitted with Hysteretic and Viscous Devices, National Technological University.

[14] IS 1893 (Part 1) - 2016 "Criteria for earthquake resistant design of structure, general provision and building", Bureau of Indian standards, New Delhi.

[15] Lorenzo Casagrandea, Innovative dampers as floor isolation systems for seismically-retrofit multi-story critical facilities, *Engineering Structures*, October 2019, pp 20 to 26.

[16] Xiaoli Wu, Seismic Performance Evaluation of Building-Damper System under Near-Fault Earthquake, *Shock and Vibration*, April 2020, pp 145 to 163.

[17] Hamdy Abou-Elfath, Periods of BRB steel buildings designed with variable seismic-force demands, *Journal of Constructional Steel Research*, 11 February 2019, pp 192 to 201.

[18] Shuling Hua, Seismic evaluation of low-rise steel building frames with self-centering energy-absorbing rigid cores designed using a force-based approach, *Engineering Structures*, December 2019, pp 123 to 143.

[19] Angelos S. Tzimas, Seismic analysis and behavior of mixed MRF/BRB regular steel space frames with uniaxial eccentricity, *Soil Dynamics and Earthquake Engineering*, March 2019, pp 31 to 35.